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AN55102 presents a Lithium-Ion (Li-Ion) battery charger design, with the smallest, low-cost PSoC® 1 device – CY8C21x23. This application note includes a dedicated PC-based software developed to perform real time charge process monitoring and analysis.

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1 Introduction

Li-Ion batteries have the greatest capacity to volume ratio and are found in notebooks, pocket PCs, cell phones, and other cutting-edge consumer products.

This application note describes a single cell Li-Ion battery charger for a 500 mAh battery using the smallest and lowest-cost chip in the PSoC family, CY8C21x23. The battery capacity and other battery parameters can easily be changed by modifying corresponding constants in the firmware to support different batteries.

Multiple methods such as, self modulated voltage reference, pin multiplexing, time multiplexing of resources, and code optimization have been used to implement the design in this chip. The charger can be embedded into consumer and home appliances or industrial applications. The production level design can be implemented in an 8-pin CY8C21123 device. The development can be done in CY8C21223 to add the digital communication required for charge monitoring.
2 PSoC Resources

Cypress provides a wealth of data at www.cypress.com to help you to select the right PSoC device for your design, and quickly and effectively integrate the device into your design. In this document, PSoC refers to the PSoC 1 family of devices. To learn more about PSoC 1, refer to the application note AN75320 - Getting Started with PSoC 1.

The following is an abbreviated list for PSoC 1:

- Overview: PSoC Portfolio, PSoC Roadmap
- Product Selectors: PSoC 1, PSoC 3, PSoC 4, or PSoC 5LP. In addition, PSoC Designer includes a device selection tool.
- Datasheets: Describe and provide electrical specifications for the PSoC 1 device family.
- Application Notes and Code Examples: Cover a broad range of topics, from basic to advanced level. Many of the application notes include code examples.
- Technical Reference Manuals (TRM): Provide detailed descriptions of the internal architecture of the PSoC 1 devices.

Development Kits:
- CY3215A-DK In-Circuit Emulation Lite Development Kit includes an in-circuit emulator (ICE). While the ICE-Cube is primarily used to debug PSoC 1 devices, it can also program PSoC 1 devices using ISSP.
- CY3210-PSOCEVAL1 Kit enables you to evaluate and experiment Cypress's PSoC 1 programmable system-on-chip design methodology and architecture.
- CY8CKIT-001 is a common development platform for all PSoC family devices.
- The MiniProg1 and MiniProg3 devices provide an interface for flash programming.

2.1 PSoC Designer

PSoC Designer is a free Windows-based Integrated Design Environment (IDE). Develop your applications using a library of pre-characterized analog and digital peripherals in a drag-and-drop design environment. Then, customize your design leveraging the dynamically generated API libraries of code. Figure 1 shows PSoC Designer windows.

Note: This is not the default view.

1. Global Resources – all device hardware settings.
2. Parameters – the parameters of the currently selected User Modules.
3. Pinout – information related to device pins.
4. Chip-Level Editor – a diagram of the resources available on the selected chip.
5. Datasheet – the datasheet for the currently selected UM
6. User Modules – all available User Modules for the selected device.
7. Device Resource Meter – device resource usage for the current project configuration.
8. Workspace – a tree level diagram of files associated with the project.
9. Output – output from project build and debug operations.

Note: For detailed information on PSoC Designer, go to PSoC® Designer > Help > Documentation > Designer Specific Documents > IDE User Guide.
2.2 Code Examples

The following webpage lists the PSoC Designer based Code Examples. These Code Examples can speed up your design process by starting you off with a complete design, instead of a blank page and also show how PSoC Designer User modules can be used for various applications.

http://www.cypress.com/go/PSoC1Code Examples

To access the Code Examples integrated with PSoC Designer, follow the path Start Page > Design Catalog > Launch Example Browser as shown in Figure 2.
In the Example Projects Browser shown in Figure 3, you have the following options.

- Keyword search to filter the projects.
- Listing the projects based on Category.
- Review the datasheet for the selection (on the Description tab).
- Review the code example for the selection. You can copy and paste code from this window to your project, which can help speed up code development, or
- Create a new project (and a new workspace if needed) based on the selection. This can speed up your design process by starting you off with a complete, basic design. You can then adapt that design to your application.

Figure 3. Code Example Projects, with Sample Codes

2.3 Technical Support

If you have any questions, our technical support team is happy to assist you. You can create a support request on the Cypress Technical Support page.

You can also use the following support resources if you need quick assistance.

- Self-help
- Local Sales Office Locations
3 Battery Charging Method

Lithium based batteries use a two-stage charge profile: activation and rapid charge stages. If the battery voltage is less than 3.0 V, it means the cell is completely discharged and the battery must be activated. In the activation stage, the battery is charged with a small constant current (typically 0.05 to 0.015 CA, where CA is the nominal battery capacity) until the battery voltage reaches the desired level. The battery activation time is limited to approximately 1.5 to 3 hours, depending on battery manufacturer recommendations. If, during activation time, the battery voltage does not rise above 3.0 V, the battery cell is considered damaged.

The rapid charge stage starts after the activation stage. Rapid charge consists of two modes: constant voltage and constant current.

When the battery voltage is less than a specified level (typically 4.2 V, but depends on battery manufacturer specifications), the charge is executed with the constant current (about 0.5 to 1 CA, depending on the battery manufacturer recommendations). When the battery voltage reaches the specified level, the charge source switches to the constant voltage mode (4.2 V). If the charge current drops below a specified limit, the charge process terminates; the battery manufacturer recommends the users to set the rapid termination current to 0.07 to 0.2 CA.

The rapid charge stage must be protected by a timeout. The constant current time is estimated to provide 100% to 120% of the battery charge because during this mode the battery is charged up to 70% to 80%. The constant voltage charge time is limited to approximately two hours, according to the manufacturer recommendations.

Figure 4 depicts the Li+ battery charge profile. Table 1 contains descriptions of the charge profile parameters and default values used in this design.

Note that Li+ batteries are very sensitive to the charge voltage, current, and discharge limit. Therefore, they are assembled with a built-in thermistor and protective circuit. This circuit protects the battery from over-charge and over-discharge, and limits the load and charge current to safe values. Without this circuit, the battery can explode under adverse conditions. The charge source voltage limit accuracy must be better than 1%.
Table 1. Example of Charge Profile Parameters and Values

<table>
<thead>
<tr>
<th>Marker</th>
<th>Parameter</th>
<th>Description</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Charging Parameters</td>
<td></td>
<td></td>
</tr>
<tr>
<td>1</td>
<td>$I_{ACT}$</td>
<td>Activation charge current</td>
<td>80 mA ± 30 mA</td>
</tr>
<tr>
<td>2</td>
<td>$I_{RAP}$</td>
<td>Rapid charge current</td>
<td>500 mA ± 40 mA</td>
</tr>
<tr>
<td>3</td>
<td>$I_{TERM}$</td>
<td>Termination current (use average of $I_{CH}$ over 1 second)</td>
<td>60 mA ±15 mA</td>
</tr>
<tr>
<td>4</td>
<td>$I_{MAX}$</td>
<td>Emergency charge stop current</td>
<td>600 mA ± 60 mA</td>
</tr>
<tr>
<td>5</td>
<td>$V_{ACT}$</td>
<td>Activation charge start voltage</td>
<td>2.0 V ± 0.1 V</td>
</tr>
<tr>
<td>6</td>
<td>$V_{RS}$</td>
<td>Rapid charge start voltage</td>
<td>3.0 V ± 0.1 V</td>
</tr>
<tr>
<td>7</td>
<td>$V_{FULL}$</td>
<td>Full charge voltage</td>
<td>4.2 V ± 0.03 V</td>
</tr>
<tr>
<td>8</td>
<td>$V_{MAX}$</td>
<td>Emergency charge stop voltage</td>
<td>4.35 V ± 0.1 V</td>
</tr>
<tr>
<td>9</td>
<td>$V_{RE-CH}$</td>
<td>Recharge voltage</td>
<td>4.0 V ± 0.1 V</td>
</tr>
<tr>
<td></td>
<td>Timing Requirements</td>
<td></td>
<td></td>
</tr>
<tr>
<td>10</td>
<td>$I_{ACT}$</td>
<td>Time limit for battery activation period</td>
<td>140 min</td>
</tr>
<tr>
<td>11</td>
<td>$I_{RAP}$</td>
<td>Time limit for constant current rapid charge period</td>
<td>80 min</td>
</tr>
<tr>
<td>12</td>
<td>$I_{VCONST}$</td>
<td>Time limit for constant voltage charge period</td>
<td>120 min</td>
</tr>
<tr>
<td>13</td>
<td>$I_{START}$</td>
<td>Maximum time for battery activation (while $V_{BATT} &lt; V_{ACT}$)</td>
<td>20 sec</td>
</tr>
<tr>
<td>14</td>
<td>$I_{TERM}$</td>
<td>Minimum time for charge complete (when $I_{CHARG} &lt; I_{TERM}$)</td>
<td>10 sec</td>
</tr>
<tr>
<td></td>
<td>Additional Parameters</td>
<td></td>
<td></td>
</tr>
<tr>
<td>15</td>
<td>$I_{MIN}$</td>
<td>Minimum current for battery health test</td>
<td>25 mA</td>
</tr>
<tr>
<td>16</td>
<td>$V_{DC_Vdd}$</td>
<td>Charger power supply voltage</td>
<td>5.2 V ± 0.2 V</td>
</tr>
</tbody>
</table>

4 Temperature Control

The charge process can be activated only if the battery temperature is within a specified limit. Typical temperature values are 0 °C to +50 °C.

Figure 5 depicts the temperature profile. Table 2 contains descriptions of the temperature profile parameters and default values used in this design.

Thermistor resistance is also used to check for the battery presence. The battery is considered disconnected when the measured thermistor resistance is greater than $R_{OPEN}$. This means there is no thermistor; therefore, no battery pack is connected. A tiered current profile, with lower current at higher temperature can be supported with modifications to the software. More information is provided in the Design Enhancements section of this application note.
Table 2. Temperature Related Parameters

<table>
<thead>
<tr>
<th>Marker</th>
<th>Parameter</th>
<th>Description</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>$T_{COLD_STOP}$</td>
<td>Stop temperature measured from battery thermistor</td>
<td>0 °C</td>
</tr>
<tr>
<td>2</td>
<td>$T_{COLD_RESTART}$</td>
<td>Restart temperature measured from battery thermistor</td>
<td>$T_{COLD_STOP} + 1$ °C</td>
</tr>
<tr>
<td>3</td>
<td>$T_{HOT_STOP}$</td>
<td>Stop temperature measured from battery thermistor</td>
<td>50 °C</td>
</tr>
<tr>
<td>4</td>
<td>$T_{HOT_RESTART}$</td>
<td>Restart temperature measured from battery thermistor</td>
<td>$T_{HOT_STOP} - 2$ °C</td>
</tr>
<tr>
<td>5</td>
<td>$R_{OPEN}$</td>
<td>Thermistor resistance limit for determining open circuit</td>
<td>40 kΩ (-7 °C)</td>
</tr>
</tbody>
</table>

5 Charger Hardware

Figure 6 shows the general structure of the charger. The following abbreviations are used within the PSoC block.

- **RS_TX**: EIA-232 (RS-232) transmitter for debug purposes (uses external transceiver). It reports temperature, voltage, and current to a PC. RS_TX is used only in the debug stage and may be removed in the released product.
- **CPU**: Central processor core for implementing charge algorithms and performing charge control functions.
- **PWM**: Pulse-width modulator for driving the regulator.
- **ADC**: Single Slope analog-to-digital converter for digitizing the analog signals.
- **AMUX**: Analog multiplexers.

The signal from the PWM goes to a low-pass RC-filter (R8 and C1). The output of the RC filter is a constant voltage signal proportional to the PWM duty cycle value. This output is connected to the base of the Q1 transistor. Therefore, the PWM with an RC-filter is a PWM-DAC. The NPN transistor Q1 is driven by an analog signal from the PWM DAC and regulates the battery charge current. The PWM period is set to 255 for accuracy, and can easily be adjusted in the firmware. The combination of Q2 and Q1 avoid reverse current, which can discharge the battery when it is still connected and the charger is turned off from the supply voltage. There is a 0.25 Ω resistor used as the current sensor. Other resistors form the battery interface to allow transformation of the battery current, voltage, and temperature into the signals that have a suitable voltage range for the PSoC analog inputs.
To correctly implement charge algorithms, the following must be measured accurately: charge current, battery voltage, and temperature. As the voltage drops on the corresponding resistors, all parameters are measured using the ADC.

To limit current flow from the battery through the interface resistors for current and voltage measurement, precision resistor dividers with large resistor values are used.

### 5.1 Low Side Current Sense

The current measurement is on the low side as shown in Figure 7, where the current flowing out of the negative terminal of battery (Node N1 to Node N2) is measured.
The current shunt resistor is outside the PSoC supply voltage to maximize and keep constant voltage range for the ADC in the PSoC. This avoids the ground being at a different potential depending on the current flow into the battery. The voltage value to be measured at Node N2 is negative with respect to PSoC, which has the ground at Node N1. Thus, a reference voltage and a summing node are required to pull this to a positive value. The reference voltage is generated using the self modulator circuit described later in this document. The advantage of this approach is that the voltage is pulled to a range higher than the offset of the ADC and thus the error due to offset can be compensated.

Precise accuracy of current measurement is necessary, when near the 4.2 V battery voltage. Therefore, during the general calibration procedure, when the transistor Q1 is off, measure the voltage bias on the current sense resistor and store it in nonvolatile memory. Subtract this memorized bias voltage from each measurement value during the normal charge process. The following equation depicts this measuring scheme:

\[
\Delta n_i = V_{\text{Charge}} \left( \frac{n_{\text{ADC max}}}{V_{\text{ADC max}}} \right) - n_{bias} \quad \text{Equation 1}
\]

\[
n_{bias} = V_{\text{ref}} \beta_{bias} \left( \frac{n_{\text{ADC max}}}{V_{\text{ADC max}}} \right) \quad \text{Equation 2}
\]

\[
V_{\text{Charge}} = I_{\text{Charge}} \beta_i \quad \text{Equation 3}
\]

Where,

- \( n_{bias} \) is the ADC code when \( I_{\text{Charge}} \) is zero
- \( \Delta n_i \) is the ADC code after removing the bias voltage and ADC offset voltage
- \( n_{\text{ADC max}} \) is full scale ADC code and the value is equal to 1023 for a 10-bit single slope ADC
- \( V_{\text{ADC max}} \) is full scale ADC voltage for the full scale ADC code
- \( I_{\text{Charge}} \) is battery charge current
- \( V_{\text{ref}} \) is self modulated reference voltage (1.3 V)
- \( \beta_{bias} \) is the resistive divider coefficient for \( V_{\text{ref}} \) (equal to 0.25 when \( R_{10} = 100 \, \text{k}\Omega \) and \( R_9 = 300 \, \text{k}\Omega \))

\[
\beta_{bias} = \left( \frac{R_{10}}{R_{10} + R_9} \right) \quad \text{Equation 4}
\]

\[
\beta_i = R_{11} \left( \frac{R_9}{R_{10} + R_9} \right) \quad \text{Equation 5}
\]
5.2 Voltage Sense

The battery voltage is scaled down to the range of the ADC10 by using the resistor divider R3 and R4 shown in Figure 8.

\[
\begin{align*}
V_{\text{Batt}} &= V_{\text{VSense}} \left( \frac{\beta V}{V_{\text{ADC max}}} \right) \\
\text{Equation 6}
\end{align*}
\]

Where,

- \( V_{\text{Batt}} \) is battery voltage.
- \( \beta V \) is the resistive divider coefficient (equal to 0.306 for \( R_3 = 22.6 \text{ k}\Omega \) and \( R_4 = 10 \text{ k}\Omega \));

\[
\beta V = \left( \frac{R_4}{R_4 + R_3} \right) \\
\text{Equation 7}
\]

The scaling is such that 4.2 V, which is the most accurate measurement required, corresponds to the 1.3 V to which the ADC10 is calibrated. The \( V_{\text{Sense}} \) voltage signal is measured by the Single Slope ADC (ADC10).

To obtain accurate voltage measurements, a calibration technique is used. The PSoC’s bandgap reference voltage error and ADC gain causes a non-calibrated voltage measurement error. The calibration procedure with external voltage reference compensates for all gain errors.

The single slope ADC is calibrated by modifying the capacitor value to obtain the expected counts for a bandgap voltage measurement, and this value is stored in flash. This value is used for every measurement cycle to calibrate the ADC to compensate for any gain errors or temperature variations. The complete details of calibration are given in a following section of this document.

5.3 Temperature Measurement

Temperature measurement is implemented with resistor R1 and the thermistor in the battery, as shown in Figure 9. The voltage \( V_T \) across the thermistor is measured with the ADC, using equations 8 and 9. The reference bias voltage \( V_{\text{ref}} \) is obtained with a self modulator circuit that is described later.
Figure 9. Temperature Measurement

Li-ion battery pack

\[ n_T = V_{\text{ref}} \beta_T \left( \frac{n_{\text{ADC max}}}{V_{\text{ADC max}}} \right) \]  

Equation 8

\[ \beta_T = \left( \frac{R_{\text{therm}}}{R_{\text{therm}} + R_1} \right) \]  

Equation 9

The thermistor transfer function is nonlinear, but there is no need to obtain the temperature value in linear units for this design. Therefore, only the temperature thresholds during the charge must be checked. This is done by analyzing the ADC code \((n_T)\). Hysteresis is added for the lower and upper bounds of the in/out temperature range to prevent multiple triggers when the temperature is close to the preset range (see Figure 5).

5.4 Self Modulator Circuit

The CY8C21x23 PSoC device does not have any analog output pins and can provide no native analog reference voltage. The self modulator circuit is formed with the comparator block and an external RC low-pass filter as shown in Figure 10.

The feedback causes the comparator output to turn ON and OFF with a duty cycle. The average voltage after the low-pass filter is equal to Vbg. This technique has a pending patent and it should be used only with Cypress products.

5.5 LED Control

An LED is used to indicate charger state. Because the project uses a small package with low pin count, the temperature sense and LED control are multiplexed. The drive mode of the pin is set to “HI-Z, Analog” when the temperature measurement is performed and to “Strong” high when the LED function is ON. All possible states displayed by the LED are described in Table 3.

Table 3. LED States

<table>
<thead>
<tr>
<th>No.</th>
<th>Charger State</th>
<th>Led State</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Charge (Activate, Rapid States)</td>
<td>ON</td>
</tr>
<tr>
<td>2</td>
<td>Charge Complete, No Battery States</td>
<td>OFF</td>
</tr>
<tr>
<td>3</td>
<td>Temperature Over Range, Battery Error</td>
<td>BLINKING</td>
</tr>
</tbody>
</table>
6 Charger Firmware

The charger firmware consists of two parts: one is the main charging functionality and the other is intended to calibrate the charger in the factory.

The main part of the firmware is built as a state machine. A diagram of the various states of the state machine is shown in Figure 11.

The order of connecting and disconnecting the three battery terminals is random. The physical ordering of the signals on the connector can vary from design to design. Therefore, all the possible sequences of Battery+, Battery-, and Thermistor connections and disconnections are allowed when a battery is installed or removed. There is no ordering that results in a lockup condition, or result in false error detection.

Figure 10. Self Modulator Circuit

Figure 11. Charger State Diagram
6.1 State Descriptions

**No Battery**: LED = OFF, no charge. Waits for the battery to be connected.

**Initialization**: LED = ON. Determines the battery presence and its state. If thermistor is present but the battery voltage value is below $V_{ACT}$, a short time battery initialization by $I_{ACT}$ current is used.

**Activation**: LED = ON. Charge by constant $I_{ACT}$ current until voltage reaches $V_{RS}$.

**Rapid Charge**: LED = ON. Constant current mode at $I_{RAP}$ until voltage reaches $V_{FULL}$. Then changes to constant voltage until current falls below $I_{TERM}$.

**Charge Complete**: LED = OFF, done charging. Wait for the battery to be removed, or for voltage to drop below $V_{RE-CH}$ to restart charge.

**Battery Error**: LED = BLINK and turn off charge. Error condition. Wait for the battery to be removed, or power cycled.

**Wait For Temperature**: LED = BLINK, stop charging. Temperature is outside of the desired range limits. Wait for the temperature to return within the limits. Then move to the Initialization state.

6.2 State Transition Descriptions

a) IF $V_{ACT} < V_{BATT} \leq V_{RE-CH}$
   THEN Activation Current
   If the battery is detected and the battery is not already charged, then turn the LED on and transition to Activation.

b) IF $V_{RS} \leq V_{BATT} < V_{MAX}$
   THEN Rapid Charge
   If the battery voltage rises above the Rapid Charge start voltage, then transition to Rapid Charge.

c) IF $V_{FULL} \leq V_{BATT} < V_{MAX}$
   AND $I_{CHARGE} \leq I_{TERM}$
   for $t_{TERM}$ seconds
   THEN Charge Complete
   If charge current falls below $I_{TERM}$ for $t_{TERM}$ seconds after the battery voltage has reached $V_{FULL}$, turn off charge current and turn off status LED and transition to Charge Complete.

d) IF $R_{THERMISTOR} \geq R_{OPEN}$
   THEN Wait for Battery
   If a battery is disconnected, then transition to No Battery.

e) IF $V_{BATT} \leq V_{RE-CH}$
   THEN Initialize the Charging Process
   If the battery voltage falls below the re-charge voltage, then transition to Initialization.

f) IF $V_{RE-CH} < V_{BATT}$
   THEN Charge Complete
   If the battery is detected and is fully charged then turn off the LED and transition to Charge Complete.

g) IF $V_{BAT} < V_{ACT}$ for $t_{ACT}$ seconds
   THEN Battery Error
   If the battery voltage is less than $V_{ACT}$ after $t_{START}$ seconds of activation current, then turn off charge current, BLINK LED, and transition to Battery Error.

h) IF $V_{BATT} \geq V_{MAX}$
   OR $I_{CHARGE} \geq I_{MAX}$
   OR Constant Current Charge Duration $> t_{RAP}$
OR Constant Voltage Charge Duration > $t_{\text{VCONST}}$

THEN Battery Error

When the battery voltage exceeds $V_{\text{MAX}}$, turn off charge current, BLINK LED, and transition to Battery Error.

If the charge current is greater than $I_{\text{MAX}}$, turn off charge current, BLINK LED, and transition to Battery Error.

If the constant current charge time is longer than $t_{\text{RAP}}$, or the constant voltage charge mode lasts longer than $t_{\text{VCONST}}$ seconds, then turn off charge current, BLINK LED, and transition to Battery Error.

i) IF $V_{\text{BATT}} \geq V_{\text{MAX}}$

OR $I_{\text{CHARGE}} \geq I_{\text{MAX}}$

OR after $t_{\text{ACT}}$ seconds: $V_{\text{BATT}} < V_{\text{RS}}$

THEN Battery Error

When battery voltage exceeds $V_{\text{MAX}}$, turn off charge current, BLINK LED, and transition to Battery Error.

If charge current is greater than $I_{\text{MAX}}$, turn off charge current, BLINK LED, and transition to Battery Error.

If the activation mode lasts longer than $t_{\text{ACT}}$ seconds, then turn off the charge current, BLINK LED, and transition to Battery Error.

When battery voltage exceeds $V_{\text{MAX}}$ and charge current is less than $I_{\text{MIN}}$ (indicating battery lead path is broken), then BLINK LED and transition to Battery Error.

j) IF $T_{\text{BATT}} \leq T_{\text{COLD\_STOP}}$

OR $T_{\text{BATT}} \geq T_{\text{HOT\_STOP}}$

THEN Temperature Outrange

When temperature reading from thermistor is out of range, turn off charge current, turn LED OFF, and transition to Wait For Temperature.

k) IF $T_{\text{BATT}} > T_{\text{COLD\_RESTART}}$

AND $T_{\text{BATT}} < T_{\text{HOT\_RESTART}}$

THEN Resume Charging

When temperature reading returns to operation range, restart charge in Initialization.

l) IF $R_{\text{THERMISTOR}} < R_{\text{OPEN}}$

THEN Initialize the Charging Process

If a battery is detected, then transition to Initialization.

6.3 Current/Voltage Control

To build a Li+ battery charger, the regulator must be capable of regulating both charge current and voltage. This charger employs a simple adaptive regulator. The regulator operation is based on increasing the PWM duty cycle if the charge voltage or charge current is smaller than the desired value. If the charge voltage or current are greater than the desired value, the PWM duty cycle is decreased. The circuit for the current control is shown in Figure 12. The PWM output is converted into a DC voltage value by using the RC low-pass filter (LPF). This voltage, when greater than the threshold voltage of transistor Q1, along with the resistor R20, determines the current in Q1 transistor. This in turn controls the current in Q2 transistor and thereby the current into the battery.
The PNP transistor Q2 also acts as a diode, preventing the battery from discharging when no power is applied to the charger. Figure 13 illustrates the regulator operation.

To obtain faster current regulation, a scheme with an adaptive step regulator is used (see Figure 14). If the regulator current is greater than the charge current by the Imis1 predefined value, the regulator step is set equal to STEP1. Current differences of Imis2 and Imis3 correspond to STEP2 and STEP3, respectively. If the difference between the target charge current and the measured current is minimum (Imis3), then the PWM step is set to ‘1’. With current difference of ImisOver, STEP_OVER is used for a fast reaction to minimize current overflow. When the battery voltage rises above 4.2 V and the FConstVoltage flag is set, the regulator step is set to ‘1’ and there is no change to the step size during the constant voltage charge period.
7 Production Calibration Procedure

As previously mentioned, all devices must be calibrated during the manufacturing process. Calibration is an easy procedure but needs a precise 4.20 V source, instead of a battery, connected to the charger connector. It also needs P1[1] (pin 4 of the ISSP connector) connected to ground as shown in Figure 15. After start, the charger is used to check the P1[1] pin. If P1[1] is externally pulled down, then the charger goes to calibration mode. P1[1] is connected to pin 4 of the ISSP connector and the PSoC ground is connected to pin 2 of ISSP connector (J2, see schematic in Appendix A: Charger Schematic for 8-pin CY8C21123). In this mode, transistors Q1 and Q2 are off, and the charger measures the constant 4.20 V. The voltage sense resistors (R3 and R4) are chosen such that 4.2 V is scaled down to 1.3 V.

The Single Slope ADC (ADC10) is calibrated with the internal bandgap voltage, which is nominally 1.3 V. Thus, scaling down 4.20 V to 1.3 V ensures accurate reading at that point. The calibration of the single slope ADC is shown in Figure 16.
The current into the CAPVAL is started at the start of an ADC conversion and a voltage ramp is generated. The comparator trips when the ramp voltage value reaches the input voltage. The Counter counts the time from the start of the current to the trip of the comparator. The PWM controls the ON and OFF times of the conversion. During PWM ON, the voltage ramp is on and the Counter counts. During PWM OFF, the capacitor is discharged and the answer is processed. The calibration function (ADCCAL) adjusts the value of CAPVAL and hence the slope of voltage ramp for full scale.

The calibration function (ADCCAL) of the ADC changes the CAPVAL capacitor value to obtain the desired ADC counts for the internal bandgap voltage. The firmware is setup to do the following:

**Step 1:** An initial ADC counts value, as shown in Equation 10, is assigned to $n_{iCAL}$.

$$n_{iCAL} = V_{bandgap} \left( \frac{n_{ADC \max}}{V_{ADC \max}} \right)$$

**Equation 10**

**Step 2:** ADC10 is calibrated with the ADCCAL function with $n_{iCAL}$ as the counts for bandgap voltage.

**Step 3:** $V_{sense}$ is measured, $n_V$ ($V_{sense} = 4.20 \text{ V}$).

**Step 4:** $n_{iCAL}$ is increased if $n_V > n_{iCAL}$ or decreased if $n_V < n_{iCAL}$.

**Step 5:** Step 2 to Step 4 is repeated till $n_V = n_{iCAL}$.

**Step 6:** $n_{iCAL}$ is stored in flash and used as the ADC calibration point for every measurement cycle.

**Step 7:** The calibration function remains in an infinite NOP loop until a reset occurs.
8 PC Utilities and Debug Information

The charger control software monitors the charge process. The program interface is simple (Figure 17). Set the COM#, press the Start button, and then turn on the charger. The software then presents the charger state and displays graphs with charge current and voltage (see Figure 17). The default values for the software must be changed to match the profile required by clicking on the “Settings”. For the project accompanying this application note (500 mA battery charger), the settings are shown in Figure 18.

Figure 17. PC Charger Monitoring Software
The charger can send two kinds of packets to the PC utility. Both packets are in text format and all values are hexadecimal. The first packet is an initialization packet that is sent once, after the charger is powered on. This package has a length of 22 bytes and contains the stored nonvolatile memory voltage thresholds that are set in the code. Packet details are represented in Table 4. The packet's structure is shown in Figure 19.

Table 4. Initialization Package

<table>
<thead>
<tr>
<th>No.</th>
<th>Length in Bytes</th>
<th>Reference</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>1</td>
<td>I</td>
<td>Character ‘I’ as start marker of initialization packet</td>
</tr>
<tr>
<td>2</td>
<td>4</td>
<td>V\text{FULL}</td>
<td>4-digit hexadecimal value of full-charge voltage (ADC code)</td>
</tr>
<tr>
<td>3</td>
<td>4</td>
<td>V\text{ACT}</td>
<td>4-digit hexadecimal value of activation start voltage (ADC code)</td>
</tr>
<tr>
<td>4</td>
<td>4</td>
<td>V\text{RS}</td>
<td>4-digit hexadecimal value of rapid start voltage (ADC code)</td>
</tr>
<tr>
<td>5</td>
<td>4</td>
<td>V\text{MAX}</td>
<td>4-digit hexadecimal value of emergency stop voltage (ADC code)</td>
</tr>
<tr>
<td>6</td>
<td>4</td>
<td>V\text{RE-CH}</td>
<td>4-digit hexadecimal value of re-charge start voltage (ADC code)</td>
</tr>
<tr>
<td>7</td>
<td>1</td>
<td>CR</td>
<td>Character with ASCII code 13 (CR) as marker of end of packet</td>
</tr>
</tbody>
</table>

Figure 19. Initialization Package Structure

```
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21
'I' V\text{FULL} V\text{ACT} V\text{RS} V\text{MAX} V\text{RE-CH} CR
```

The second packet is sent regularly and contains the current state of the charger battery voltage, charger current, temperature values, and errors. Using this packet, the PC utility builds charts and displays actual battery parameters. This packet has a length of 16 bytes. Packet details are represented in Table 5. The packet's structure is shown in Figure 20.
The program in the PSoC does not calculate the actual current and voltage in amperes and volts. It only looks at ADC counts and makes state machine decisions based on them. The PC utility calculates the amperes and volts for debugging purposes.

Table 5. Information Packet

<table>
<thead>
<tr>
<th>No.</th>
<th>Length in Bytes</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>1</td>
<td>Character with ASCII code 10 (LF) as packet start marker</td>
</tr>
<tr>
<td>2</td>
<td>1</td>
<td>Charger State</td>
</tr>
<tr>
<td></td>
<td></td>
<td>0 – Initialization</td>
</tr>
<tr>
<td></td>
<td></td>
<td>1 – Battery Activation</td>
</tr>
<tr>
<td></td>
<td></td>
<td>2 – Rapid Charge</td>
</tr>
<tr>
<td></td>
<td></td>
<td>3 – Charge Complete</td>
</tr>
<tr>
<td></td>
<td></td>
<td>4 – Error</td>
</tr>
<tr>
<td></td>
<td></td>
<td>5 – Temperature Outrange</td>
</tr>
<tr>
<td></td>
<td></td>
<td>6 – No Battery Charger</td>
</tr>
<tr>
<td>3</td>
<td>1</td>
<td>Errors</td>
</tr>
<tr>
<td></td>
<td></td>
<td>0 – No Error</td>
</tr>
<tr>
<td></td>
<td></td>
<td>1 – Voltage Error (V_{BAT} \geq V_{MAX})</td>
</tr>
<tr>
<td></td>
<td></td>
<td>2 – Current Error (I_{CH} \geq I_{MAX})</td>
</tr>
<tr>
<td></td>
<td></td>
<td>3 – Activation Timeout</td>
</tr>
<tr>
<td></td>
<td></td>
<td>4 – Constant Current Rapid Charge Stage Timeout</td>
</tr>
<tr>
<td></td>
<td></td>
<td>5 – Constant Voltage Rapid Charge Stage Timeout</td>
</tr>
<tr>
<td></td>
<td></td>
<td>6 – Battery Initialization Timeout</td>
</tr>
<tr>
<td>4</td>
<td>4</td>
<td>4-digit hexadecimal value of charge current (I_{\text{CHARGE}}) ADC code</td>
</tr>
<tr>
<td>5</td>
<td>4</td>
<td>4-digit hexadecimal value of battery voltage (V_{\text{BATT}}) ADC code</td>
</tr>
<tr>
<td>6</td>
<td>4</td>
<td>4-digit hexadecimal value of voltage drop on thermistor used for temperature control</td>
</tr>
<tr>
<td>7</td>
<td>1</td>
<td>Character with ASCII code 13 (CR) as marker of end of packet</td>
</tr>
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</table>

Figure 20. Information Package Structure

<table>
<thead>
<tr>
<th>0</th>
<th>1</th>
<th>2</th>
<th>3</th>
<th>6</th>
<th>7</th>
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<th>11</th>
<th>14</th>
<th>15</th>
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<tbody>
<tr>
<td>LF</td>
<td>State</td>
<td>Error</td>
<td>I_{\text{CHARGE}}</td>
<td>V_{\text{BATT}}</td>
<td>T</td>
<td>CR</td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

9 Design Enhancements

The project accompanying this application note is for designs with no voltage feedback regulation. The current into the battery is thus limited by the power dissipation in transistor Q2. The charger in this application note is designed to support batteries with a capacity up to 500 mAh.

9.1 Higher Charge Capacity Battery Charger

To charge batteries of higher capacity the options are: use an expensive PNP transistor with a higher power rating or incorporate a feedback mechanism to decrease the voltage drop across current control PNP transistor (Q2) as shown in Figure 21. In a complete system, the feedback control can be a fly-back circuit, which does the voltage regulation.
10 Multicell Battery Charger

To implement a multicell battery charger, the Vdd to PSoC must be regulated for the entire range of voltages (all batteries discharged to fully charged). The voltage regulation across current control PNP transistor (Q2) is required to facilitate higher current flow.

10.1 Tiered Charge Profile

This is straightforward to implement with the current project. The state machine can be easily modified to get a different charge profile. A tiered rapid charge mode could be created that is dependent on the temperature by modifying the state machine. Since the different states are well defined in the firmware, it is easy to add or modify a few conditional statements to change the profile.

About the Author

Name: Archana Yarlagadda
Title: Application Engineer
Background: Applications Engineer in Cypress with focus on PSoC applications. Masters in Analog VLSI from University of Tennessee, Knoxville
11 Appendix A: Charger Schematic for 8-pin CY8C21123
12 Appendix B: Charger Schematic for 16-pin CY8C21223
## Appendix C: Charger BOM for CY8C21123/CY8C21223

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<th>Description</th>
<th>Quantity</th>
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<td>C1, C2, C3, C4, C5, C6</td>
<td>0.1 uF</td>
<td>PCC1762CT-ND</td>
<td>Capacitor 0.1 uF X7R 0603</td>
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<tr>
<td>D1</td>
<td></td>
<td>67-1552-1-ND</td>
<td>LED</td>
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<tr>
<td>DZ1</td>
<td></td>
<td>MMBZ5226B-FDICT-ND</td>
<td>Zener Diode</td>
<td>1</td>
</tr>
<tr>
<td>J2</td>
<td></td>
<td>WM4203-ND</td>
<td>ISSP Connector 5 pin 100 mil partially shrouded</td>
<td>1</td>
</tr>
<tr>
<td>J1</td>
<td></td>
<td></td>
<td>2 pin header</td>
<td>1</td>
</tr>
<tr>
<td>Q1</td>
<td></td>
<td>MMBT5089LT1GOSCT-ND</td>
<td>BJT - NPN</td>
<td>1</td>
</tr>
<tr>
<td>Q2</td>
<td></td>
<td>568-4167-1-ND</td>
<td>BJT – PNP</td>
<td>1</td>
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<tr>
<td>R1, R4</td>
<td>10K</td>
<td>P10.0KHCT-ND</td>
<td>Resistor 10K 1% 0603</td>
<td>2</td>
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<tr>
<td>R2</td>
<td>1K</td>
<td>P1.00KHCT-ND</td>
<td>Resistor 1K 1% 0603</td>
<td>1</td>
</tr>
<tr>
<td>R3</td>
<td>22K6</td>
<td>P22.6KHCT-ND</td>
<td>Resistor 22K6 1% 0603</td>
<td>1</td>
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<tr>
<td>R5</td>
<td>100 Ohms</td>
<td>P100HCT-ND</td>
<td>Resistor 100 Ohms 1% 0603</td>
<td>1</td>
</tr>
<tr>
<td>R6</td>
<td>39 Ohms</td>
<td>P39.0HCT-ND</td>
<td>Resistor 39 Ohms 1% 0603</td>
<td>1</td>
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<tr>
<td>R7, R8</td>
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<td>P3.90KHCT-ND</td>
<td>Resistor 3K9 1% 0603</td>
<td>2</td>
</tr>
<tr>
<td>R9</td>
<td>100K</td>
<td>P100KHCT-ND</td>
<td>Resistor 100K 1% 0603</td>
<td>1</td>
</tr>
<tr>
<td>R10</td>
<td>300K</td>
<td>P300KHCT-ND</td>
<td>Resistor 300K 1% 0603</td>
<td>1</td>
</tr>
<tr>
<td>R11, R12, R13, R14</td>
<td>1 Ohms</td>
<td>P1.0DCT-ND</td>
<td>Resistor 1 Ohms 1/8 Watt 0805 1%</td>
<td>4</td>
</tr>
</tbody>
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14 Appendix D: Firmware Flow Chart
## Document History

**Document Title:** AN55102 – PSoC® 1 Single Cell Li-Ion Battery Charger with CY8C21x23  
**Document Number:** 001-55102

<table>
<thead>
<tr>
<th>Revision</th>
<th>ECN</th>
<th>Orig. of Change</th>
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<tr>
<td>**</td>
<td>2752862</td>
<td>YARA</td>
<td>08/18/2009</td>
<td>New application note</td>
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| *A       | 3210386   | YARA            | 03/30/2011      | 1. Modified the schematic to show the 8-pin implementation  
2. Added BOM for 8 pin implementation  
3. Updated the project to PD 5.1  
4. Updated the Title and Abstract.  
5. Added a folder called Charge Control Center, which was earlier accessible through AN2267, to make this AN stand-alone. |
| *B       | 3271365   | YARA            | 06/01/2011      | Document title updated as per template.                                                |
| *C       | 3510163   | RJVB            | 01/27/2012      | Schematic and block diagram updated  
Updated project with PD5.2  
Updated template |
| *D       | 3704640   | DESH            | 08/06/2012      | No change. Completing sunset review.                                                   |
| *E       | 4764533   | ASRI            | 05/14/2015      | Updated Schematic diagram for CY8C21123  
Added Schematic diagram for CY8C21223  
Updated project with PD5.4  
Updated template |
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